



Current Source for Diode Testing

INTRODUCTION

A programmable current source that was designed for biasing diodes under test is easier to set to the required current than a conventional current source.

The current source, designed for testing Hewlett-Packard PIN diodes, is programmed by thumb wheel switches in 10 μ A steps, from 10 μ A to 700 mA with an accuracy better than $\pm 1\%$. Changes in current settings may be made quickly without a current monitor.

APPLICATIONS

This current source is ideal as a bias source in diode test set-ups since the current may be set accurately without any additional equipment.

It may be used either to set a particular bias current or to determine what current is required to obtain certain parameter values which vary with current.

It has been used in RF resistance test set-ups, for biasing detectors, PIN switches, and attenuators, and in various diode circuits for checking intermodulation and cross modulation distortion.

CIRCUIT DESCRIPTION

Figure 1 is a block diagram of the current source and Figures 2, 3, 4, and 5 are detailed schematics of each section.

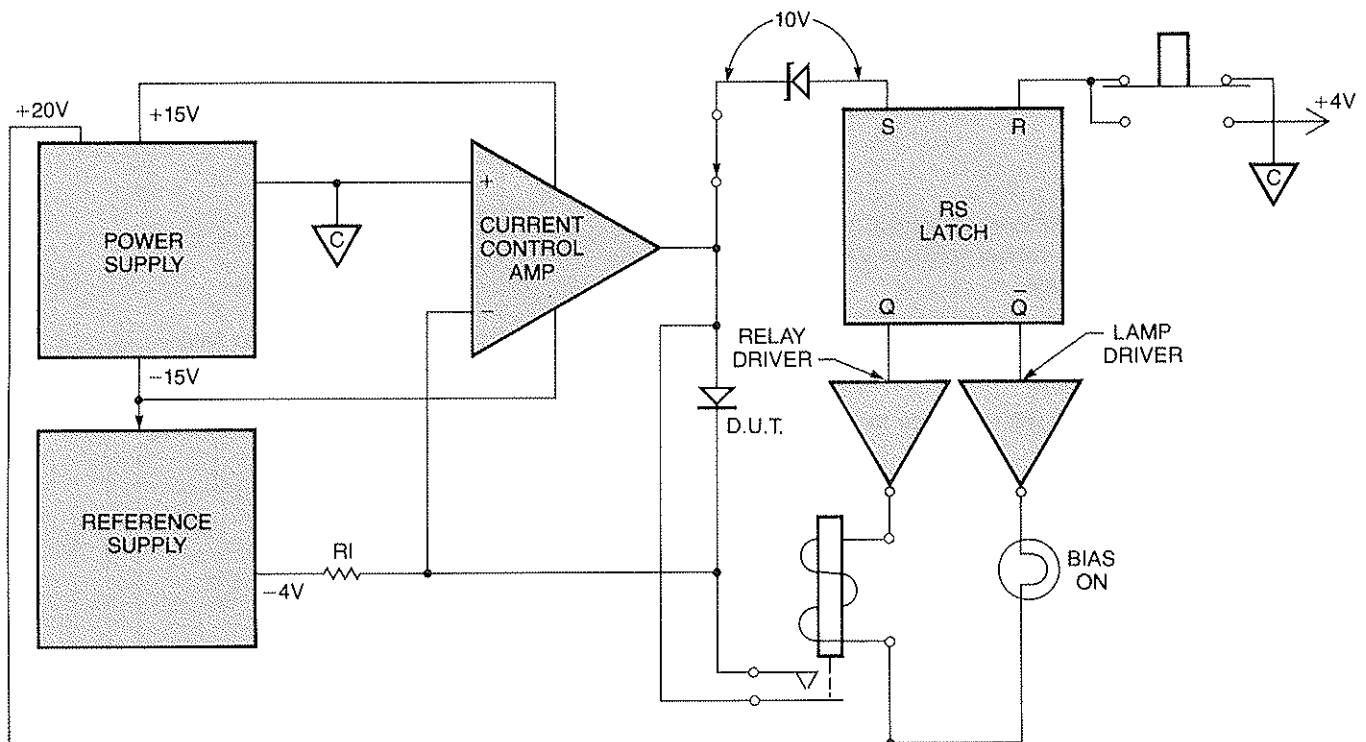


Figure 1. Current Source .

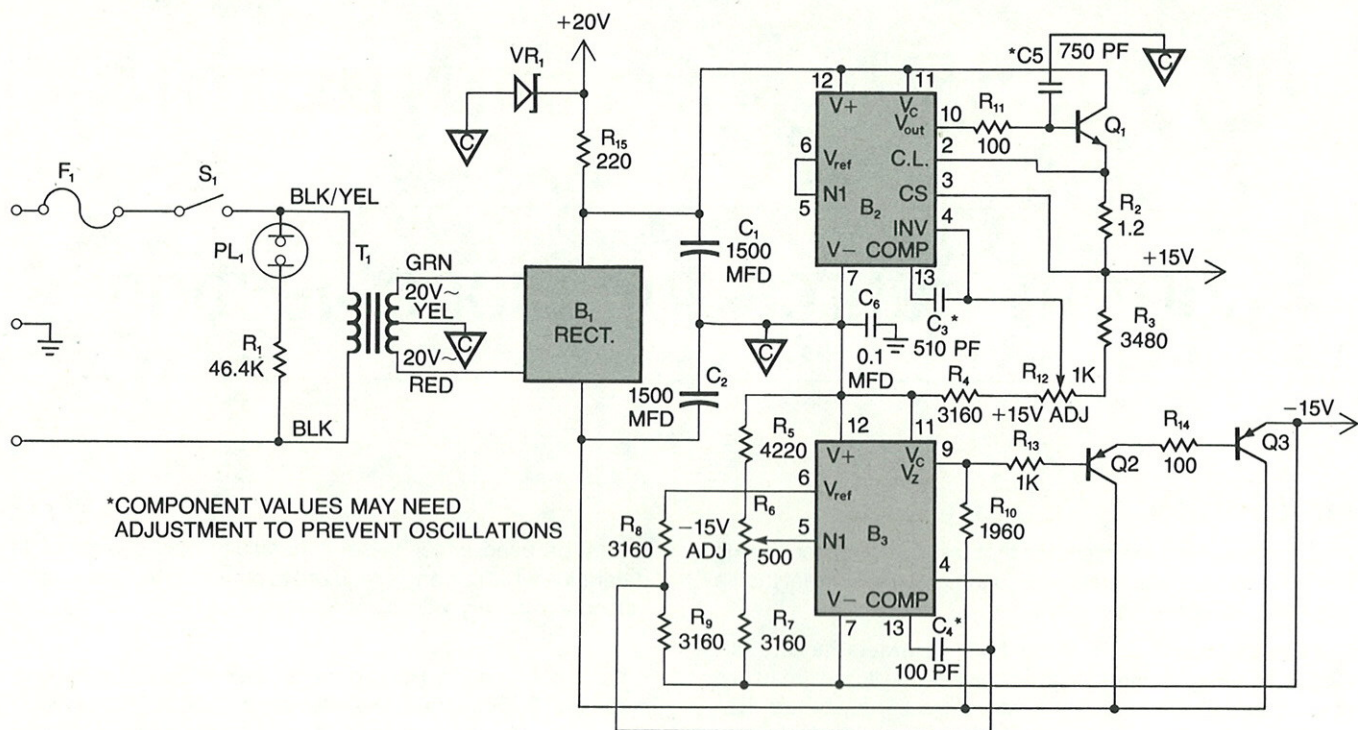


Figure 2. Power Supply.

POWER SUPPLY

The power supply (Figure 2) has a 1 amp transformer and a 1 amp bridge rectifier furnishing power to two Fairchild 723 PC voltage regulators for a regulated $\pm 15V$. A zener regulator furnishes +20V for the "current on" lamp and output shorting relay in Figure 5.

The components marked with an asterisk in Figures 2 and 3 may need to be adjusted to prevent oscillation of the voltage supplies.

REFERENCE SUPPLY

The accuracy of the reference supply (Figure 3) combined with the accuracy of the current control resistors determines the accuracy of the current source.

The reference supply is controlled by a Motorola MC 1439G operational amplifier and with an input from -15 volt supply provides a regulated -4 volts.

Zener VR2 furnishes a +10 volt reference for the regulator.

CURRENT CONTROL AMPLIFIER

The current control amplifier (Figure 4) also uses a Motorola MC 1439G with FET's at the inputs to keep leakage current to less than 1 nA.

The MC 1439G controls a current driver consisting of two cascaded emitter followers.

The entire circuit is an operational amplifier with R_i (input resistance) being the selected combination of 0.1% resistors R_{23} through R_{41} and R_f (feedback resistance) being the load on the output. The input current is determined by $R_i/4$ volts and since leakage of the FET is negligible the input current is also the output current to the load.

Q6 and Q7 should be selected for a voltage match of 100 mV or better with 20K resistors on the source, gates at 0 volts and $V_{DD} = +15V$, $V_{SS} = -15V$.

Both sides of the output float and either polarity may be grounded in use.

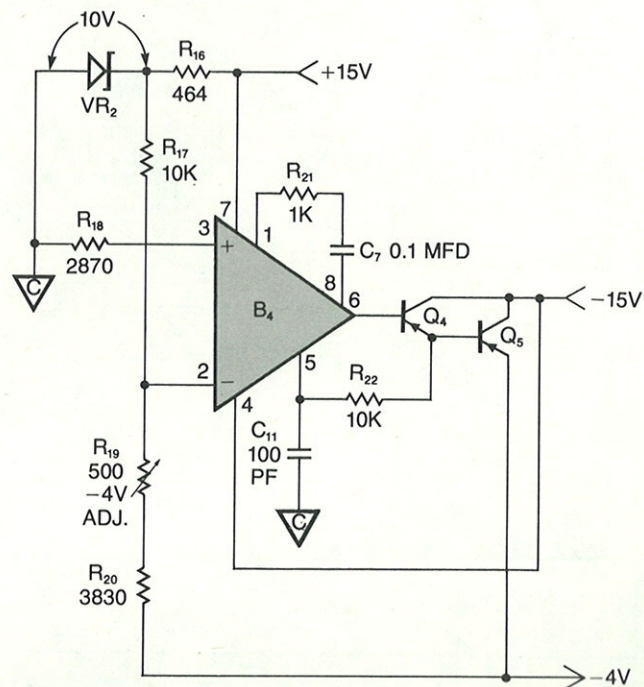


Figure 3. Reference Supply.

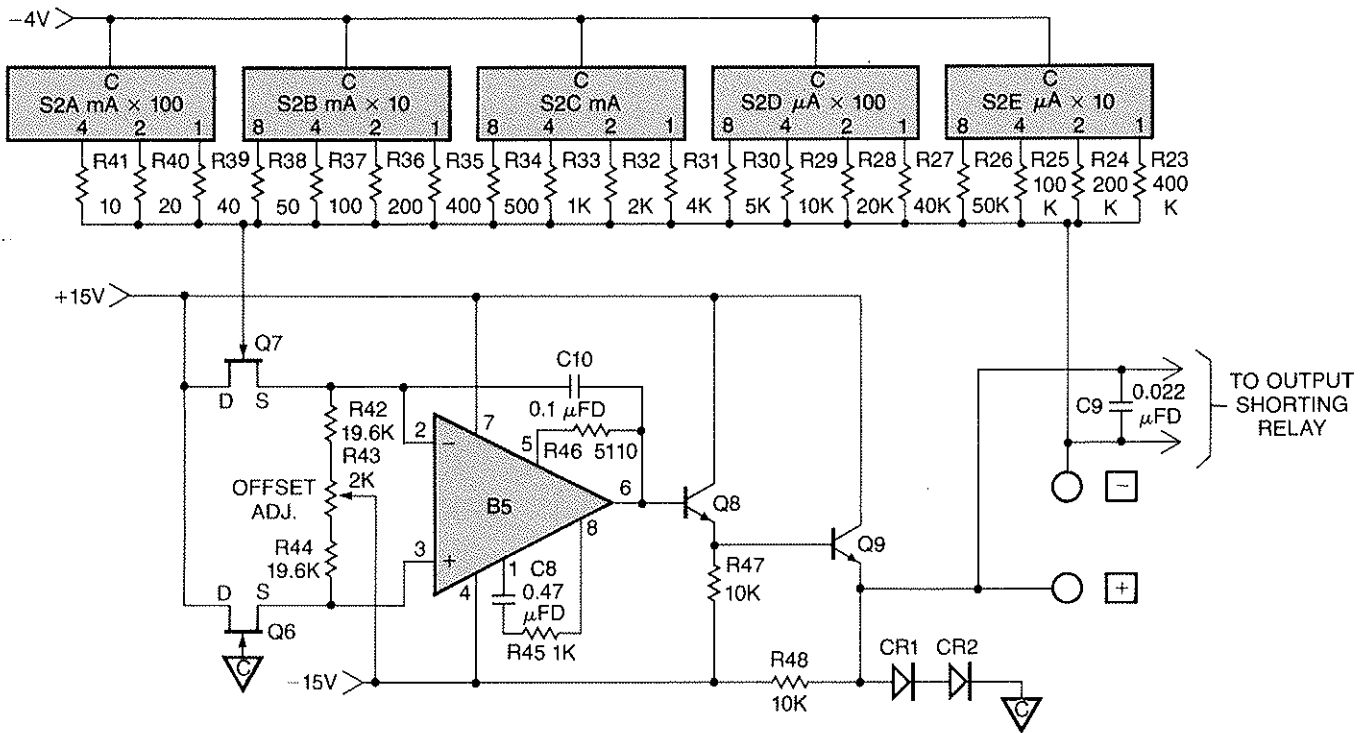


Figure 4. Current Control Amplifier.

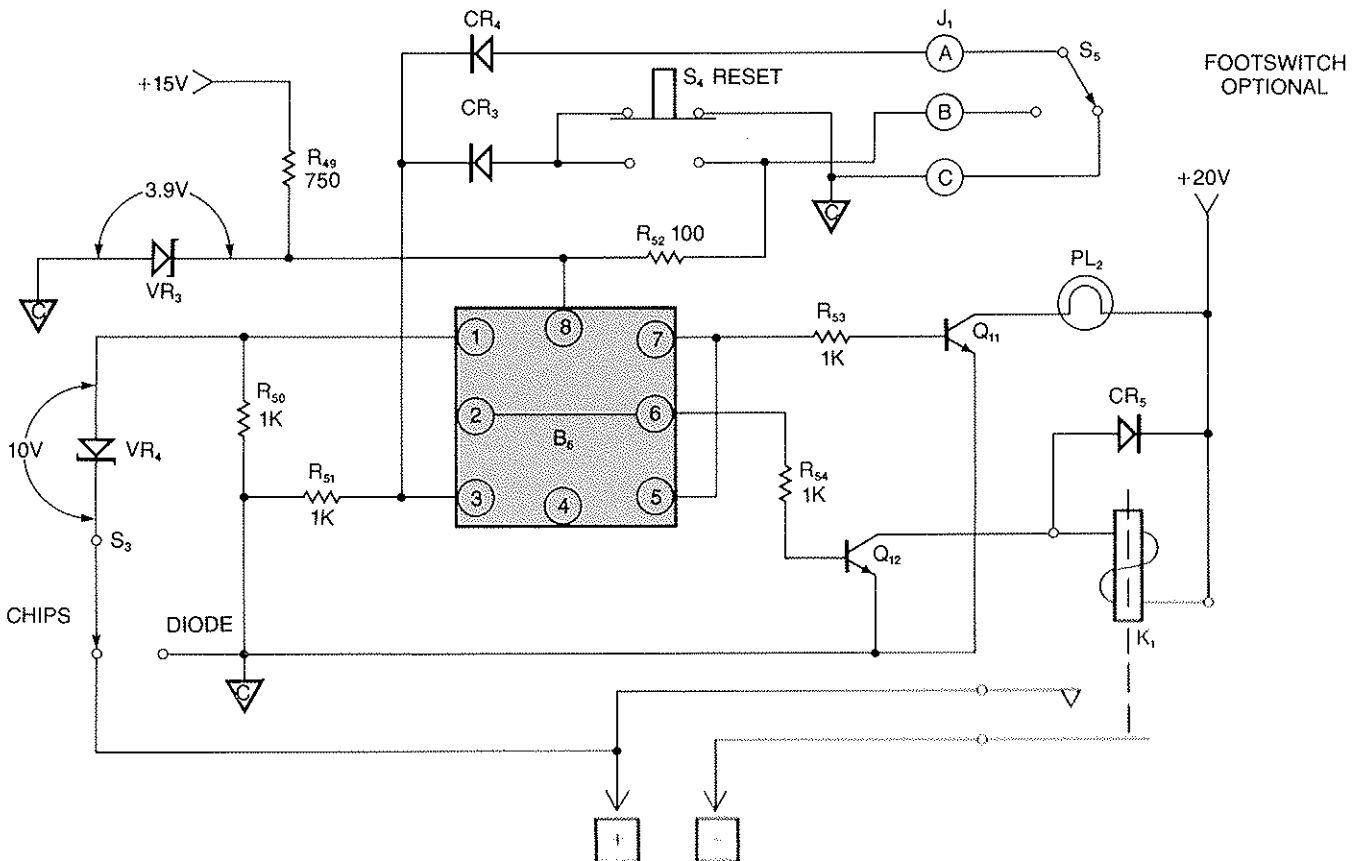


Figure 5. Output Shorting Circuit.

OUTPUT SHORTING CIRCUIT

The output shorting circuit is a safety feature which prevents the probe from welding to the chip when testing diode chips. It is also useful for testing diodes which may be burned out by the application of the current source open circuit voltage — approximately 14 volts.

When switch S3 is in the "CHIPS" position an open circuit is sensed through zener VR4 which sets RF (Set-Reset) latch B6 closing relay K1 and turning off the current on light PL-2. After a diode is placed across the output the latch is reset by momentary push button switch S4 or an optional foot switch.

ASSEMBLY

The only precautions necessary in assembly are the AC wiring should be separated from the other wiring and the chassis must be well grounded with a 3-conductor power cord.

CALIBRATION

With output terminals shorted and current set to 20 mA, adjust ± 15 volt supplies to 15 volt $\pm 1\%$ and -4 volts supply to 4 volts $\pm 0.1\%$.

Set current to 10 μA leaving output shorted. Then adjust offset balance for a reading of 0.0 ± 10 mV between current terminals and power supply common.

The current at each setting of the current switches should now be within 1% of setting. If not, replace or pad the appropriate resistor to correct it.

MATERIAL LIST FOR CURRENT SOURCE

B1	RECTIFIER BRIDGE MOTOROLA MDA-920	Q3,5	TRANSISTOR, FET, 2N4856	R34	RESISTOR, 500, $\frac{1}{8}W$, 0.1%
B2,3	VOLTAGE REGULATOR FAIRCHILD 723 PC	Q8	TRANSISTOR, 2N4239	R35	RESISTOR, 400, $\frac{1}{8}W$, 0.1%
B4,5	OPERATIONAL AMPLIFIER MOTOROLA MC 1439G	Q10,11	TRANSISTOR, 2N3417	R36	RESISTOR, 200, $\frac{1}{8}W$, 0.1%
B6	DUAL 2 INPUT NOR GATE FAIRCHILD 9914	R1	RESISTOR, 46.4K, $\frac{1}{8}W$	R37	RESISTOR, 100, $\frac{1}{8}W$, 0.1%
C1,2	CAPACITOR, 1500 MFD, 50V	R2	RESISTOR, 1.2 Ω , 1W	R38	RESISTOR, 50, $\frac{1}{2}W$, 0.1%
C3	CAPACITOR, 510 PFD	R3	RESISTOR, 3.48K, $\frac{1}{8}W$	R39	RESISTOR, 40, $\frac{1}{2}W$, 0.1%
C4	CAPACITOR, 100 PFD	R4,8,9	RESISTOR, 3.16K, $\frac{1}{8}W$	R40	RESISTOR, 20, 1W, 0.1%
C5	CAPACITOR, 750 PFD	R5	RESISTOR, 422K, $\frac{1}{8}W$	R41	RESISTOR, 10, 2W, 0.1%
C6,7	CAPACITOR, 0.1 MFD	R6,19	RESISTOR, VAR, 500 Ω	R42,44	RESISTOR, 19.6K, $\frac{1}{8}W$
C8	CAPACITOR, 0.47 MFD	R7	RESISTOR, 1.21K, $\frac{1}{8}W$	R43	RESISTOR, 2K
C9	CAPACITOR, 1 MFD, 25V CERAMIC	R10	RESISTOR, 1.96K, $\frac{1}{8}W$	R46	RESISTOR, 5.11K, $\frac{1}{8}W$
C10	CAPACITOR, 0.1 MFD	R11,14,52	RESISTOR, 100 Ω , $\frac{1}{8}W$	R49	RESISTOR, 750, $\frac{1}{8}W$
C11	CAPACITOR, 100 PFD	R12	RESISTOR, VAR, 1K	S1	SWITCH, LIGHTED, P.B. OAK 53-67280-121-A1H
CR1-5	DIODE-SWITCHING FAIRCHILD FD2225	R13,21,45, 50,51,53,54	RESISTOR, 1K, $\frac{1}{8}W$	S2	THUMBWHEEL SWITCH, 5 POLE, 1-2-4-8 BCD DIGITRAN 378-5
F1	FUSE, 1A, 250V	R15	RESISTOR, 220 Ω	S3	SWITCH, TOGGLE, SPDT ALCO MST-205N
J1	CONNECTOR, 3 PIN AMPHENOL, MS3102A-10SL-3P (OPTIONAL)	R16	RESISTOR, 464 Ω	S4	SWITCH, SPDT, PUSHBUTTON, MOMENTARY C&K 8121
J2	BINDING POSTS H.H. SMITH 1814 RB	R17,22,48	RESISTOR, 10K, $\frac{1}{8}W$	S5	FOOTSWITCH, SPDT (OPTIONAL)
K1	RELAY, SPST MAGNECRAFT W102MPCX-8	R18	RESISTOR, 2887K, $\frac{1}{8}W$	T1	TRANSFORMER TRIAD F-92A
P1	PLUG, 3 PIN AMPHENOL MS3106A-10SL-3S (OPTIONAL)	R20	RESISTOR, 3.83K, $\frac{1}{8}W$	VR1	DIODE, ZENER, 20V, 1W, 1N4747
PL1	PILOT LIGHT, PART OF S1	R23	RESISTOR, 400K, $\frac{1}{8}W$, 0.1%	VR2,4	DIODE, ZENER, 10V, 0.4W, 1N758A
PL2	LAMP, 18V DRAKE 10-607	R24	RESISTOR, 200K, $\frac{1}{8}W$, 0.1%	VR3	DIODE, ZENER, 3.9V, 0.4W, 1N748A
Q1,9	TRANSISTOR, 2N3054	R25	RESISTOR, 100K, $\frac{1}{8}W$, 0.1%	XB2,3	SOCKET DIP, 14 PIN
Q2,4	TRANSISTOR, 2N1132	R26	RESISTOR, 50K, $\frac{1}{8}W$, 0.1%	XB4,5,6	SOCKET, 8 PIN, IC, ROUND
		R27	RESISTOR, 40K, $\frac{1}{8}W$, 0.1%	XF1	FUSEHOLDER - PANEL MOUNT
		R28	RESISTOR, 20K, $\frac{1}{8}W$, 0.1%	XP2	HOUSING - INDICATOR LAMP SYLVANIA SM-1
		R29	RESISTOR, 10K, $\frac{1}{8}W$, 0.1%		
		R30	RESISTOR, 5K, $\frac{1}{8}W$, 0.1%		
		R31	RESISTOR, 4K, $\frac{1}{8}W$, 0.1%		
		R32	RESISTOR, 2K, $\frac{1}{8}W$, 0.1%		
		R33	RESISTOR, 1K, $\frac{1}{8}W$, 0.1%		
					POWER CORD 3 CONDUCTOR



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